

- 1 -

METHOD FOR PRODUCING A SILICON NITRIDE FILTER

The present invention relates to a method for producing a silicon nitride filter suitable for removing dust, etc. contained in a high temperature exhaust gas.

5        Silicon nitride has excellent characteristics with respect to heat resistance, corrosion resistance, chemical resistance, strength, etc., and is expected to be useful as a filter for dust arresting or dust removing in a high temperature or corrosive environment, or as a  
10       filter for cleaning the exhaust gas from a diesel engine. Methods for producing such silicon nitride filters have been proposed.

For example, JP-A-6-256069 proposes a method which comprises mixing coarse silicon nitride particles and a  
15       glass powder, followed by molding and baking. However, such a method wherein a low melting point material is added as a binder, has a problem that the heat resistance of silicon nitride will be substantially impaired. Further, JP-A-7-187845 and JP-A-8-59364 propose methods  
20       wherein a mixture of silicon nitride particles and an

organic silicon compound, and a mixture of silicon  
nitride particles and a polysilazane, are used,  
respectively, as starting materials, and molded products  
are likewise baked. However, an organic silicon compound  
5 such as a polysilazane is usually expensive, and the  
methods of using such expensive materials have a problem  
with respect to the production cost and the availability  
of the starting materials.

On the other hand, as a method for obtaining a  
10 silicon nitride filter by using inexpensive metal silicon  
particles instead of silicon nitride particles and  
carrying out nitriding treatment, JP-A-1-188479 proposes  
a method to obtain a filter having a nitriding ratio of  
silicon nitride particles of at most 50%, by using as a  
15 starting material, a mixed powder comprising metal  
silicon particles and silicon nitride particles.  
However, in this method, the nitriding ratio of the  
silicon nitride particles is at most 50%, whereby there  
will be a substantial amount of metal silicon particles  
20 remaining in the silicon nitride sintered product without  
being nitrided, whereby the excellent heat resistance and  
corrosion resistance of silicon nitride are likely to be  
impaired.

It is an object of the present invention to provide  
25 a method for producing a silicon nitride filter having  
high strength and being most suitable for arresting and  
removing dusts, using silicon nitride particles as a

starting material.

In a first aspect, the present invention provides a method for producing a silicon nitride filter, which comprises heat-treating in nitrogen a green body  
5 comprising from 35 to 90 mass% of silicon nitride particles having an average particle diameter of from 1 to 30 $\mu$ m, from 5 to 60 mass% of a pore-forming agent and from 0.1 to 5 mass% of metal oxide particles, provided that the total amount of the silicon nitride particles,  
10 the pore-forming agent and the metal oxide particles is at least 90 mass%, to form a porous product made substantially of silicon nitride.

In a second aspect, the present invention provides a method for producing a silicon nitride filter, which  
15 comprises heat-treating in nitrogen a green body comprising from 45 to 85 mass% of silicon nitride particles having an average particle diameter of from 1 to 30 $\mu$ m, from 10 to 50 mass% of metal oxide hollow particles and from 0.1 to 5 mass% of metal oxide solid  
20 particles, provided that the total amount of the silicon nitride particles, the metal oxide hollow particles and the metal oxide solid particles is at least 90 mass%, to form a porous product made substantially of silicon nitride.

25 Now, the present invention will be described in detail with reference to the preferred embodiments.

In the method for producing a silicon nitride filter

of the present invention (hereinafter referred to as the present production method), a green body comprising from 5 to 60 mass% (hereinafter referred to simply as %) of a pore-forming agent, from 35 to 90% of silicon nitride particles having an average particle diameter of from 1 to 30  $\mu\text{m}$  and from 0.1 to 5% of metal oxide particles, is used.

In the present production method, the content of the pore-forming agent is from 5 to 60% in the green body.

10 If the content is less than 5%, the proportion of pores to perform a filter function tends to be inadequate. On the other hand, if the content exceeds 60%, no adequate strength tends to be obtained, although the porosity of the filter becomes large. The content of the pore-

15 forming agent is preferably from 15 to 40% in the green body, whereby the filter can be made to have high strength and a high porosity.

Further, if the pore-forming agent is spherical, pores to be formed, will also be spherical, whereby

20 deterioration in strength can be suppressed even when the porosity is increased. Further, when the pore-forming agent is spherical, the average particle diameter is preferably from 20 to 200  $\mu\text{m}$ . If the average particle diameter of the pore-forming agent is less than 20  $\mu\text{m}$ ,

25 the average pore diameter of the silicon nitride filter obtainable after the heat treatment, will be at most 5  $\mu\text{m}$ , such being undesirable. On the other hand, if it

exceeds 200  $\mu\text{m}$ , the average pore diameter of the silicon nitride filter obtainable after the heat treatment, tends to exceed 20  $\mu\text{m}$ , such being undesirable as a filter for removing dust or the like.

5       The pore-forming agent is not particularly limited so long as it forms pores. The pore-forming agent may, for example, be one which flies upon e.g. decomposition during heat treatment, to form pores, or oxide hollow particles. The pore-forming agent is preferably organic  
10   polymer particles, particularly heat decomposable polymer particles, whereby it will be decomposed and dissipated during the heat treatment and thus leaves no residue in the sintered product, whereby the properties of the silicon nitride filter thereby obtainable, will not be  
15   impaired. The present production method wherein the pore-forming agent is organic polymer particles, will be hereinafter referred to as the present production method 1.

      In the present production method 1, the organic  
20   polymer may, for example, be a polyvinyl alcohol, an acrylic resin, a vinyl acetate resin or cellulose. If the organic polymer particles added as the pore-forming agent will remain in a substantial amount as carbon without being sufficiently thermally decomposed during  
25   the temperature rise in heat treatment, silicon carbide is likely to form in the subsequent heat treating step, thus leading to clogging of pores, such being

undesirable. From this viewpoint, it is preferred to use acrylic resin particles as the pore-forming agent, since it is readily thermally decomposable, and the amount remaining as carbon will be small. The average particle  
5 diameter of the organic polymer particles is preferably from 20 to 100  $\mu\text{m}$ .

In the present production method, oxide hollow particles may be used as the pore-forming agent. The present production method wherein the pore-forming agent  
10 is oxide hollow particles, will be hereinafter referred to as the present production method 2.

As the metal oxide hollow particles (hereinafter referred to simply as hollow particles), any particles may be suitably used so long as they are metal oxide  
15 particles capable of forming pores during the heat treatment, but in the present invention, the metal oxide hollow particles refer to metal oxide particles having a porosity of at least 30%. If the porosity is less than 30%, the ability to form pores tends to be inadequate.  
20 The porosity of the hollow particles is preferably from 40 to 80%, more preferably from 50 to 70%.

The hollow particles preferably contain, as the main component, an oxide of Al and/or Si, since it is effective to increase the porosity due to gasification of  
25 the component, or to improve the oxidation resistance by solid solubilization of a part of the component.

The hollow particles may have a dense or porous

outer skin, so long as they are hollow. Further, the hollow particles are preferably spherical particles on appearance, whereby they are readily available. However, they may be particles other than spherical particles, so long as they are hollow.

The average particle diameter of the hollow particles is preferably from 30 to 200  $\mu\text{m}$ , whereby the porosity of the filter to be obtained, will be large, and the strength will also be secured. If the average particle diameter of the hollow particles is less than 30  $\mu\text{m}$ , the contribution to formation of pores tends to decrease. On the other hand, if the average particle diameter exceeds 200  $\mu\text{m}$ , the strength of the filter tends to be inadequate, such being undesirable.

The content of the hollow particles is preferably from 10 to 50% in the green body. If the content is less than 10%, the proportion of pores to perform the filter function, tends to be inadequate. On the other hand, if the content exceeds 50%, no adequate strength tends to be obtainable, although the porosity of the filter increases.

The silicon nitride particles to be used in the present production method, have an average particle diameter of from 1 to 30  $\mu\text{m}$ . If the average particle diameter of the silicon nitride particles is less than 1  $\mu\text{m}$ , the amount of absorption of moisture or oxygen of the external air e.g. during the preparation of the green

body, increases and the amount of silicon dioxide formed by oxidation of silicon nitride particles tends to be too large. Further, if the average particle diameter of the silicon nitride particles exceeds 30  $\mu\text{m}$ , spherical pores  
5 can not be formed as a final filter, whereby the strength characteristics will deteriorate. The average particle diameter of the silicon nitride particles is more preferably from 1 to 10  $\mu\text{m}$ .

The purity of the silicon nitride particles is  
10 suitably selected depending upon the particular purpose and application.

The content of the silicon nitride particles is usually from 35 to 90% in the green body. If the content is less than 35%, it tends to be difficult to obtain a  
15 filter having high heat resistance while maintaining sufficient strength. On the other hand, if the content exceeds 90%, the content of the pore-forming agent becomes small, and the porosity can not be made sufficiently large. The content of the silicon nitride  
20 particles is preferably from 50 to 80% in the green body. In the present production method 2, the content of the silicon nitride particles is preferably from 45 to 85% in the green body.

As the metal oxide particles to be used in the  
25 present production method, it is preferred to employ particles containing, as the main component, an oxide of at least one metal selected from the group consisting of



Al, Ca, Sr, Ba, Y, Mg and Yb, whereby a sintering aid effect can be obtained, and high strength can be secured. The metal oxide particles may be, in addition to the metal oxide particles themselves, an organic metallic  
5 compound which becomes metal oxide particles after thermal decomposition.

The metal oxide particles preferably have a fine particle size, and the average particle diameter is preferably at most 10  $\mu\text{m}$ , whereby the particles can be  
10 dispersed uniformly in the filter in a small amount. By the addition of the metal oxide particles, the silicon nitride portion to form pores will have a dense structure, and the pores to be formed, will be spherical.

The content of the metal oxide particles is from 0.1  
15 to 5%. If the content of the metal oxide particles is less than 0.1% in the green body, the structure of the silicon nitride matrix as a backbone can not be made sufficiently dense, whereby high strength can not be obtained. Further, if the content exceeds 5% in the  
20 green body, the heat resistance of silicon nitride tends to be impaired, such being undesirable.

In the present production method 2, the metal oxide particles are preferably metal oxide solid particles (hereinafter referred to simply as solid particles). In  
25 the present specification, the solid particles represent metal oxide particles having a porosity of less than 30%.

In the present production method 2, the green body

preferably comprises from 45 to 85% of silicon nitride particles having an average particle diameter of from 1 to 30  $\mu\text{m}$ , from 10 to 50% of the hollow particles, and from 0.1 to 5% of the solid particles.

5 In this production method, the total amount of the pore-forming agent, the silicon nitride particles and the metal oxide particles, is at least 90% in the green body. If the total amount of the pore-forming agent, the silicon nitride particles and the metal oxide particles,  
10 is less than 90% in the green body, it will be difficult to obtain a filter having the desired properties.

In the present production method, as a method for preparing a green body comprising the pore-forming agent, the silicon nitride particles and the metal oxide  
15 particles, a common ceramic-forming method such as press molding, extrusion molding or slip casting, may suitably be employed. Further, at the time of molding, an organic binder may be added separately from the pore-forming agent. As such an organic binder, an organic substance  
20 such as polyvinyl alcohol or its modified product, starch or its modified product, carboxymethyl cellulose, hydroxymethyl cellulose, polyvinyl pyrrolidone, an acrylic resin or an acrylic copolymer, a vinyl acetate resin or a vinyl acetate copolymer, may, for example, be  
25 employed. The amount of such an organic binder is preferably from 1 to 10 parts by mass per 100 parts by mass of the green body. Further, the pore-forming agent

may serve also as a binder for the green body.

As a condition for the heat treatment of the above green body, the heat treatment is carried out in a nitrogen atmosphere. As a condition for heat treatment,  
5 it is preferred to maintain it in a nitrogen atmosphere at a temperature of from 1,450 to 1,800°C. If the temperature range is less than 1,450°C, sintering of the silicon nitride particles tends to hardly proceed, such being undesirable. On the other hand, if it exceeds  
10 1,800°C, the silicon nitride particles tend to be decomposed, such being undesirable. In the present production method 2, it is preferred to maintain the green body in a nitrogen atmosphere at a temperature of from 1,600 to 1,800°C.

15 The retention time is preferably from 1 to 12 hours. If the retention time is less than 1 hour, bonding of the particles to one another may not sufficiently proceed. On the other hand, if it exceeds 12 hours, silicon nitride is likely to be decomposed especially at a high  
20 temperature, such being undesirable. The retention time is more preferably from 2 to 5 hours.

The temperature raising rate in the heat treatment is suitably selected depending upon the size, shape, etc. of the green body. However, in a dewaxing step,  
25 decomposed gas will be formed in a large amount, and the temperature raising rate is preferably from 50 to 200°C/hr.

Here, the nitrogen atmosphere is meant for an atmosphere comprising substantially nitrogen only and containing no oxygen. However, it may contain other inert gas. The nitrogen partial pressure is preferably  
5 at least 50 kPa.

The porosity of the silicon nitride filter obtained by the present production method is preferably from 30 to 80%. The porosity is measured by an Archimedean method. If the porosity is less than 30%, the pressure loss tends  
10 to be large, such being undesirable as a filter. On the other hand, if the porosity exceeds 80%, the strength tends to be low, such being undesirable as a filter.

The average pore diameter as measured by a mercury immersion method of the silicon nitride filter obtained  
15 by the present production method is preferably from 5 to 40  $\mu\text{m}$ . If the average pore diameter is less than 5  $\mu\text{m}$ , the pressure loss during the use of the filter tends to be large, such being undesirable. If the average pore diameter exceeds 40  $\mu\text{m}$ , arresting and removing fine  
20 exhaust particles such as diesel particulates tend to be difficult, such being undesirable. The average pore diameter is more preferably from 5 to 20  $\mu\text{m}$ .

Now, the present invention will be described in further detail with reference to Examples (Examples 1 to  
25 6, 9 and 14 to 16) and Comparative Examples (Examples 7, 8, 10 to 13, and 17 and 18). The pore characteristics were measured by a mercury porosimeter (Auto SCAN-33,

tradename, manufactured by Yuasa Ionics K.K.), and the thermal expansion coefficient was measured by a differential thermal expansion measuring apparatus (tradename: TAS-100, manufactured by Rigaku K.K.) within  
5 a range of from room temperature to 1,000°C.

#### EXAMPLE 1

To 68 parts by mass of silicon nitride particles having an average particle diameter of 5  $\mu\text{m}$ , 30 parts by mass of spherical acrylic resin particles having an  
10 average particle diameter of 20  $\mu\text{m}$  and 2 parts by mass of powdery magnesium oxide particles were added, and using ethyl alcohol as a dispersing medium, mixing was carried out for two hours by ball-milling method. After drying, this mixed powder was filled in a press mold of 60 mm  $\times$   
15 60 mm and press-molded under a molding pressure of 19.6 MPa to obtain a green body having a thickness of 10 mm. This green body was heated from room temperature to 500°C at a rate of 60°C/hr and from 500°C to 1,760°C at a rate of 400°C/hr and maintained at 1,760°C for 4 hours for  
20 heat treatment in a nitrogen atmosphere in an atmosphere-controllable electric furnace.

The characteristics of the obtained sintered product were such that the porosity was 60%, and the average pore diameter was 8  $\mu\text{m}$ . With respect to this sintered  
25 product, the thermal expansion coefficient was measured and found to be low at a level of  $2.9 \times 10^{-6}/^\circ\text{C}$ . Further, from the sintered product, a bending test specimen having

a size of 4 mm × 3 mm × 40 mm was cut out, and the three point bending strength with a span of 30 mm was measured at room temperature. The load applying rate was 0.5 mm/min. As a result, the bending strength was high at a level of 40 MPa. The structure of the sintered product was observed to be such that the silicon nitride matrix was dense, and spherical pores formed by the acrylic resin, were uniformly dispersed therein.

#### EXAMPLE 2

The operation was the same as in Example 1 except that the retention time at 1,760°C was changed from 4 hours to one hour. The characteristics of the obtained sintered product were such that the porosity was 65%, the average pore diameter was 9.5 μm, and the thermal expansion coefficient was  $3.0 \times 10^{-6}/^{\circ}\text{C}$ . Further, the three point bending strength at room temperature measured in the same manner as in Example 1, was 25 MPa. The structure of the sintered product was observed to be such that the silicon nitride matrix was dense, and spherical pores formed by the acrylic resin, were uniformly dispersed therein.

#### EXAMPLE 3

The operation was the same as in Example 1 except that the acrylic resin particles having an average particle diameter of 20 μm were changed to vinyl acetate resin particles having an average particle diameter of 60 μm. The characteristics of the obtained sintered product

were such that the porosity was 59%, and the average pore diameter was 20  $\mu\text{m}$ . Further, the three point bending strength at room temperature measured in the same manner as in Example 1, was 20 MPa. The structure of the  
5 sintered product was observed to be such that the silicon nitride matrix was dense, and spherical pores formed by the vinyl acetate resin particles, were uniformly dispersed therein.

#### EXAMPLE 4

10 The operation was the same as in Example 1 except that the amount of the silicon nitride particles was changed to 48 parts by mass, the amount of the acrylic resin particles was changed to 50 parts by mass, and the amount of the powdery magnesium oxide particles was  
15 changed to 2 parts by mass. The characteristics of the obtained sintered product were such that the porosity was 80%, the average pore diameter was 15  $\mu\text{m}$ , and the thermal expansion coefficient was  $3.1 \times 10^{-6}/^{\circ}\text{C}$ . Further, the three point bending strength at room temperature measured in  
20 the same manner as in Example 1, was 5 MPa. The structure of the sintered product was observed to be such that the silicon nitride matrix was dense, and spherical pores formed by the acrylic resin, were uniformly dispersed therein.

#### 25 EXAMPLE 5

To 60 parts by mass of silicon nitride particles having an average particle diameter of 5  $\mu\text{m}$ , 35 parts by

mass of acrylic resin particles having an average particle diameter of 100  $\mu\text{m}$  and 5 parts by mass of powdery yttrium oxide particles were added, and using ethyl alcohol as a dispersing medium, mixing was carried out for two hours by ball-milling method. After drying, this mixed powder was filled in a press mold of 60 mm  $\times$  60 mm, and press-molded under a molding pressure of 19.6 MPa to obtain a green body having a thickness of 10 mm. This green body was heated from room temperature to 1,000°C at a rate of 60°C/hr and from 1,000 to 1,700°C at a rate of 400°C/hr and maintained at 1,700°C for 4 hours for heat treatment in a nitrogen atmosphere in an atmosphere-controllable electric furnace.

The characteristics of the obtained sintered product were such that the porosity was 65%, the average pore diameter was 20  $\mu\text{m}$ , and the thermal expansion coefficient was  $3.1 \times 10^{-6}/^\circ\text{C}$ . Further, the three point bending strength at room temperature measured in the same manner as in Example 1, was 10.9 MPa. The structure of the sintered product was observed to be such that the silicon nitride matrix was dense, and spherical pores formed by the acrylic resin, were uniformly dispersed therein.

#### EXAMPLE 6

To 65 parts by mass of silicon nitride particles having an average particle diameter of 1.5  $\mu\text{m}$ , 30 parts by mass of acrylic resin particles having an average particle diameter of 50  $\mu\text{m}$  and 5 parts by mass of powdery



spinel particles ( $\text{MgAl}_2\text{O}_4$ ) were added, and using ethyl alcohol as a dispersing medium, mixing was carried out for two hours by ball-milling method. After drying, this mixed powder was filled in a press mold of 60 mm × 60 mm, and press-molded under a molding pressure of 19.6 MPa to obtain a green body having a thickness of 10 mm. This green body was heated from room temperature to 500°C at a rate of 60°C/hr and from 500 to 1,750°C at a rate of 400°C/hr and maintained at 1,750°C for two hours for heat treatment in a nitrogen atmosphere in an atmosphere-controllable electric furnace.

The characteristics of the obtained sintered product were such that the porosity was 60%, the average pore diameter was 12  $\mu\text{m}$ , and the thermal expansion coefficient was  $3.1 \times 10^{-6}/^\circ\text{C}$ . Further, the three point bending strength at room temperature measured in the same manner as in Example 1, was 10.8 MPa. The structure of the sintered product was observed to be such that the silicon nitride matrix was dense, and spherical pores formed by the acrylic resin, were uniformly dispersed therein.

#### EXAMPLE 7

The operation was the same as in Example 1 except that the metal oxide particles were not added. The characteristics of the obtained sintered product were such that the porosity was 75%, the average pore diameter was 12  $\mu\text{m}$ , and the thermal expansion coefficient was  $3.0 \times 10^{-6}/^\circ\text{C}$ . Further, the three point bending strength at

room temperature measured in the same manner as in Example 1, was low at a level of 8 MPa. The structure of the sintered product was observed to be such that the silicon nitride matrix was porous, and spherical pores  
5 formed by the acrylic resin, were dispersed therein.

#### EXAMPLE 8

To 100 parts by mass of metal silicon particles having an average particle diameter of 50  $\mu\text{m}$ , 30 parts by mass of acrylic resin particles having an average  
10 particle diameter of 50  $\mu\text{m}$  were added, and using ethyl alcohol as a dispersing medium, mixing was carried out for two hours by ball-milling method. After drying, this mixed powder was filled in a press mold of 60 mm  $\times$  60 mm, and press-molded under a molding pressure of 19.6 MPa to  
15 obtain a green body having a thickness of 10 mm. This green body was heated from room temperature to 500°C at a rate of 60°C/hr and from 500 to 1,600°C at a rate of 400°C/hr and maintained at 1,600°C for 4 hours for heat treatment in a nitrogen atmosphere in an atmosphere-  
20 controllable electric furnace.

The characteristics of the obtained sintered product were such that the porosity was 60% and the average pore diameter was 20  $\mu\text{m}$ . However, in the obtained sintered products, a substantial amount of silicon metal residue  
25 was observed, and its thermal expansion coefficient was high at a level of  $4.0 \times 10^{-6}/^\circ\text{C}$ . The three point bending strength at room temperature measured in the same manner

as in Example 1, of this sample, was 9 MPa.

#### EXAMPLE 9

To 68 parts by mass of silicon nitride particles having an average particle diameter of 5  $\mu\text{m}$ , 30 parts by mass of alumina hollow particles (porosity: 50%) having an average particle diameter of 75  $\mu\text{m}$  and 2 parts by mass of MgO solid particles having an average particle diameter of 2  $\mu\text{m}$ , were added, and using ethanol as a dispersing medium, wet mixing was carried out for 30 minutes by ball-milling method. The mixture was finally dried.

The obtained mixed particles were filled in a press mold of 60 mm  $\times$  60 mm, and uniaxially press-molded under a molding pressure of 20 MPa to obtain a green body. The green body was heated from room temperature to 1,000°C at a rate of 100°C/hr and maintained at 1,000°C for two hours and then heated from 1,000°C to 1,760°C at a rate of 300°C/hr and maintained at 1,760°C for 4 hours for heat treatment in a nitrogen atmosphere in an electric furnace.

The characteristics of the obtained sintered product were such that the porosity was 50% and the average pore diameter was 20  $\mu\text{m}$ . With respect to this porous product, the crystal phase was identified by X-rays, whereby only silicon nitride was observed. The structure of the porous product was observed to be such that the matrix portion was well densified, and spherical pores formed by

the hollow particles were uniformly dispersed. With respect to this porous product, the thermal expansion coefficient was measured and found to be low at a level of  $3.0 \times 10^{-6}/^{\circ}\text{C}$  within a range of from room temperature to 1,000°C. Further, from the sintered product, a bending test specimen having a size of 4 mm × 3 mm × 40 mm was cut out, and the three point bending strength with a span of 30 mm was measured at room temperature. The load applying rate was 0.5 mm/min. As a result, the bending strength was high at a level of 70 MPa.

#### EXAMPLE 10

The operation was the same as in Example 9 except that in Example 9, the silicon nitride particles were changed from 68 parts by mass to 43 parts by mass, and the amount of the alumina hollow particles was changed from 30 parts by mass to 110 parts by mass. The obtained sintered product had a porosity of 85% and an average pore diameter of 45 μm. The structure of the porous product was observed to be such that the matrix portion was well densified, and spherical pores formed by hollow particles were uniformly dispersed. With respect to this porous product, the X-ray diffraction, the thermal expansion coefficient measurement and the three point bending strength measurement were carried out in the same manner as in Example 9. As a result, in the identification of the crystal phase, a peak of alumina was observed in addition to a peak of silicon nitride.

Further, the thermal expansion coefficient was high at a level of  $5.3 \times 10^{-6}/^{\circ}\text{C}$  within a range of from room temperature to  $1,000^{\circ}\text{C}$ . The three point bending strength at room temperature was 3 MPa.

5   EXAMPLE 11

10       The operation was the same as in Example 9 except that in Example 9, the silicon nitride particles were changed from 68 parts by mass to 62 parts by mass, and the amount of the MgO solid particles was changed from 2 parts by mass to 8 parts by mass. The obtained sintered product had a porosity of 20% and an average pore diameter of 8  $\mu\text{m}$ . With respect to this porous product, the X-ray diffraction, the thermal expansion coefficient measurement and the three point bending strength  
15   measurement were carried out in the same manner as in Example 9. As a result, in the identification of the crystal phase, a peak of spinel ( $\text{MgAl}_2\text{O}_4$ ) was observed. Further, the thermal expansion coefficient was  $4.0 \times 10^{-6}/^{\circ}\text{C}$  within a range of from room temperature to  $1,000^{\circ}\text{C}$ . The  
20   three point bending strength at room temperature was 250 MPa. Further, the structure of the obtained sintered product was observed to be such that the matrix portion was well densified, and spherical pores formed by the hollow particles were uniformly dispersed, but a  
25   remarkable modification was observed. This is believed attributable to the fact that sintering was remarkably promoted by the formed liquid phase.

EXAMPLE 12

The operation was the same as in Example 9 except that in Example 9, the average particle diameter of the silicon nitride particles was changed from 5  $\mu\text{m}$  to 50  $\mu\text{m}$ .

5 The obtained sintered product had a porosity of 75% and an average pore diameter of 40  $\mu\text{m}$ , and sintering and densification of the structure did not proceed at all. With respect to this porous product, the X-ray diffraction, the thermal expansion coefficient  
10 measurement and the three point bending strength measurement were carried out in the same manner as in Example 9. As a result, in the identification of the crystal phase, peaks of silicon nitride and alumina were observed. Further, the thermal expansion coefficient was  
15 low at a level of  $4.0 \times 10^{-6}/^{\circ}\text{C}$  within a range of from room temperature to 1,000 $^{\circ}\text{C}$ . The three point bending strength at room temperature was low at a level of 6 MPa.

EXAMPLE 13

The operation was the same as in Example 9 except  
20 that in Example 9, the silicon nitride particles were changed to metal silicon. With respect to this porous product, the X-ray diffraction, the thermal expansion coefficient measurement and the three point bending strength measurement were carried out in the same manner  
25 as in Example 9. As a result, the obtained sintered product had a porosity of 70% and an average pore diameter of 45  $\mu\text{m}$ . Further, the crystal phase was

identified, whereby a peak of silicon nitride was observed. With respect to this porous product, the thermal expansion coefficient was measured and found to be low at a level of  $3.1 \times 10^{-6}/^{\circ}\text{C}$  within a range of from  
5 room temperature to  $1,000^{\circ}\text{C}$ . However, the structure of the porous product was observed to be such that spherical pores formed by the hollow particles were uniformly dispersed in the porous silicon nitride structure, and the three point bending strength at room temperature was  
10 low at a level of 5 MPa.

#### EXAMPLE 14

To 72 parts by mass of silicon nitride particles having an average particle diameter of  $5\text{ }\mu\text{m}$ , 35 parts by mass of silica hollow particles (porosity: 70%) having an  
15 average particle diameter of  $100\text{ }\mu\text{m}$  and 3 parts by mass of  $\text{Y}_2\text{O}_3$  solid particles were dry-mixed for 30 minutes by a mixer. The obtained mixed particles were uniaxially press-molded in the same manner as in Example 9 to obtain a green body. The green body was heated from room  
20 temperature to  $500^{\circ}\text{C}$  at a rate of  $100^{\circ}\text{C/hr}$  and from  $500^{\circ}\text{C}$  to  $1,600^{\circ}\text{C}$  at a rate of  $300^{\circ}\text{C/hr}$  and maintained at  $1,600^{\circ}\text{C}$  for 5 hours for heat treatment in a nitrogen atmosphere in an electric furnace.

The obtained sintered product were such that the  
25 porosity was 60% and the average pore diameter was  $30\text{ }\mu\text{m}$ . The structure of the porous product was observed to be such that the matrix portion was well densified, and

spherical pores formed by the hollow particles were uniformly dispersed. With respect to this porous product, the crystal phase was identified by X-rays, whereby only silicon nitride was observed. And, the thermal coefficient was measured and found to be low at a level of  $3.1 \times 10^{-6}/^{\circ}\text{C}$  within a range of from room temperature to  $1,000^{\circ}\text{C}$ . The three point bending strength at room temperature was high at a level of 60 MPa.

#### EXAMPLE 15

10 To 67 parts by mass of silicon nitride particles having an average particle diameter of  $10\text{ }\mu\text{m}$ , 30 parts by mass of mullite type glass hollow particles (porosity: 50%) having an average particle diameter of  $45\text{ }\mu\text{m}$  and 3 parts by mass of  $\text{Yb}_2\text{O}_3$  solid particles, were added, and  
15 ethanol was further added as a dispersing medium, followed by wet mixing for 30 minutes by ball-milling method. The mixture was finally dried. The obtained mixed particles were uniaxially press-molded in the same manner as in Example 9 to obtain a green body. The green  
20 body was heated from room temperature to  $1,100^{\circ}\text{C}$  at a rate of  $200^{\circ}\text{C/hr}$  and maintained at  $1,100^{\circ}\text{C}$  for two hours and then heated from  $1,100^{\circ}\text{C}$  to  $1,700^{\circ}\text{C}$  at a rate of  $60^{\circ}\text{C/hr}$  and maintained at  $1,700^{\circ}\text{C}$  for 5 hours for heat  
25 furnace.

The characteristics of the obtained sintered product were such that the porosity was 50% and the average pore



diameter was 15  $\mu\text{m}$ . The structure of the porous product was observed to be such that the matrix portion was well densified, and spherical pores formed by the hollow particles were uniformly dispersed. With respect to this porous product, the thermal expansion coefficient was measured and found to be low at a level of  $2.9 \times 10^{-6}/^{\circ}\text{C}$  within a range of from room temperature to  $1,000^{\circ}\text{C}$ , and the three point bending strength at room temperature was 100 MPa.

10 EXAMPLE 16

To 63 parts by mass of silicon nitride particles having an average particle diameter of 20  $\mu\text{m}$ , 35 parts by mass of silica-alumina hollow particles (porosity: 70%) having an average particle diameter of 50  $\mu\text{m}$  and 2 parts by mass of  $\text{Y}_2\text{O}_3$  solid particles, were added, followed by dry-mixing by a mixer. To 100 parts by mass of this mixed particles, 10 parts by mass of methyl cellulose and 10 parts by mass of deionized water were added and sufficiently kneaded by a kneader to obtain an extrusion molding material, followed by extrusion molding. The obtained extrusion molded green body was dried in a hot air dryer, and then heated from room temperature to  $800^{\circ}\text{C}$  at a rate of  $50^{\circ}\text{C}/\text{hr}$  and maintained at  $800^{\circ}\text{C}$  for two hours, then heated from  $800^{\circ}\text{C}$  to  $1,700^{\circ}\text{C}$  at a rate of  $60^{\circ}\text{C}/\text{hr}$  and maintained at  $1,700^{\circ}\text{C}$  for 5 hours, for heat treatment in a nitrogen atmosphere in an electric furnace.

The obtained sintered product had a porosity of 60% and an average pore diameter of 18  $\mu\text{m}$ . The structure of the porous product was observed to be such that the matrix portion was well densified, and spherical pores  
5 formed by the hollow particles were uniformly dispersed. Identification of the crystal phase was carried out by X-rays, whereby only silicon nitride was observed. Further, with respect to this porous product, the thermal coefficient was measured and found to be low at a level  
10 of  $2.9 \times 10^{-6}/^{\circ}\text{C}$  within a range of from room temperature to  $1,000^{\circ}\text{C}$ . The three point bending strength at room temperature was 60 MPa.

#### EXAMPLE 17

To 93 parts by mass of silicon nitride particles  
15 having an average particle diameter of 2  $\mu\text{m}$ , 5 parts by mass of  $\text{Y}_2\text{O}_3$  solid particles having an average particle diameter of 2  $\mu\text{m}$  and 2 parts by mass of aluminum oxide solid particles having an average particle diameter of 1.5  $\mu\text{m}$ , were added. Further, 50 parts by mass of  
20 deionized water and 0.1 part by mass of polycarboxylic acid type dispersing agent to the particles, were added to prepare a slurry. A polyurethane foamed resin body of 60 mm  $\times$  60 mm  $\times$  30 mm was dipped in the slurry and deaerated under vacuum, whereupon the polyurethane foamed  
25 resin body was taken out and dried.

After the drying, it was sintered in a nitrogen atmosphere at  $1,800^{\circ}\text{C}$  for 4 hours in an electric furnace.

After the sintering, the obtained silicon nitride filter had a porosity of 75%, but large pores having an average pore diameter of 100  $\mu\text{m}$ , were formed, and the three point strength at room temperature was also low at a level of 8  
5 MPa. Further, identification of the crystal phase was carried out by the X-ray diffraction, whereby a peak of silicon carbide was observed in addition to a peak of silicon nitride.

#### EXAMPLE 18

10 Into toluene, 100 parts by mass of silicon nitride particles having an average particle diameter of 1  $\mu\text{m}$  and 300 parts by mass of polysilazane were added and thoroughly stirred to obtain a slurry. The prepared slurry was dried, then the obtained particles were  
15 pulverized, and further, the particle size was adjusted to obtain molding particles. The molding particles were uniaxially press-molded in the same manner as in Example 9, and then subjected to isostatic pressing (CIP) under 100 MPa. After the molding, it was heated from room  
20 temperature to 500°C at a rate of 6 °C/hr and from 500°C to 1,200°C at a rate of 300°C/hr and maintained at 1,200°C for 6 hours, and then further heated from 1,200°C to 1,400°C at a rate of 100°C/hr and maintained at 1,400°C for 4 hours, for heat treatment.

25 The obtained sintered product had a porosity of 87% and an average pore diameter of 35  $\mu\text{m}$ . Cracks of about 10  $\mu\text{m}$  were present at various portions of the sintered

product. With respect to this porous product,  
identification of the crystal phase was carried out by X-  
rays, whereby the presence of silicon nitride and mullite  
was observed. With respect to this porous product, the  
5 three point bending strength at room temperature was  
measured and found to be low at a level of 5 MPa.

By the present production method, a silicon nitride  
filter suitable for dust arresting or dust removing can  
easily be produced. The silicon nitride filter obtained  
10 by the present invention has an average pore diameter  
which is most suitable for arresting diesel particulates,  
and the porosity is larger than the conventional product,  
and yet, the strength is sufficient, and corrosion  
resistance is excellent. Accordingly, when it is used  
15 for removal of diesel particulates, it presents a diesel  
particulate filter which has a high particulate arresting  
rate and which is excellent also in durability.

The entire disclosures of Japanese Patent  
Application No. 2000-313955 filed on October 13, 2000 and  
20 Japanese Patent Application No. 2000-313956 filed on  
October 13, 2000 including specifications, claims and  
summaries are incorporated herein by reference in their  
entireties.